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*Published in:*  
2015 IEEE International Topical Meeting on Microwave Photonics

*Link to article, DOI:*  
[10.1109/MWP.2015.7356674](https://doi.org/10.1109/MWP.2015.7356674)

*Publication date:*  
2015

*Document Version*  
Peer reviewed version

[Link back to DTU Orbit](#)

*Citation (APA):*  
Rommel, S., Cavalcante, L. C. P., Vegas Olmos, J. J., Tafur Monroy, I., & Mishra, A. K. (2015). Requirements for Bend Insensitive Fiber in Millimeter-Wave Fronthaul Systems. In *2015 IEEE International Topical Meeting on Microwave Photonics* IEEE. <https://doi.org/10.1109/MWP.2015.7356674>

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# Requirements for Bend Insensitive Fiber in Millimeter-Wave Fronthaul Systems

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**Abstract**—The impact of fiber bending on mm-wave radio-over-fiber transmission is investigated and the need for bend insensitive fiber for front-haul installation confirmed. A 70m W-band hybrid photonic-wireless link including bend insensitive fiber is demonstrated with  $BER < 10^{-6}$  at 5mm bending radius.

## I. INTRODUCTION

The increasing use of bandwidth intensive applications on mobile consumer devices such as smartphones and tablet computers has created a demand for high-speed wireless data communications at gigabit speeds that need to be supported by future 5G mobile networks. Millimeter-wave (mm-wave) radio-over-fiber (RoF) links have been identified as a key candidate for the required mobile front- and backhaul as well as direct gigabit-class wireless broadband services [1]–[5], as a viable alternative to baseband, digitized, packet encapsulated grey optic solutions [5], [6].

RoF links in the different mm-wave bands have been demonstrated with wireless transmission distances ranging from a few to multiple hundred meters and with a variety of optical generation, upconversion and radio-frequency (RF) detection setups [4], [7], [8]. The transmission fiber itself has received attention mostly with regard to transmission impairments due to dispersion and fiber nonlinearities [9] or the combination of single- and multi-mode fibers [7] and—more recently—as a means for capacity increase by combining spatial multiplexing in the fiber with the well known concept of multiple-input multiple-output (MIMO) RF transmission [3].

The practical consideration of on-premise fiber installation and optical wiring of—and within—the antenna has however been neglected, although it is obvious that—analogue to the case of fiber-to-the-x [10]—fiber bends with small radii are likely to occur. With the introduction of MIMO transmission and antenna arrays especially as well as their housing in compact, weather resistant and easy to mount outdoor units, radii well below 10 mm will be common and macrobending induced losses may thus play a significant role.

In this paper we assess the performance of a W-band RoF link with 15 km optical and 70 m wireless transmission. Significantly we include 5 km of bend insensitive fiber (BIF), we show that for radii below 15 mm BIF is a necessity and demonstrate how the use of different fibers from the set of

specifications defined by ITU-T G.657 may allow different numbers of bends at different radii. Finally we discuss the trade-off between the available power budget, required tolerance to fiber bending and the cost of including BIF.

## II. EXPERIMENTAL SETUP

The experimental setup is depicted in Fig. 1 and employs photonic upconversion at the transmitter, consisting of an external cavity laser (ECL) at  $\lambda = 1550$  nm for signal generation, followed by a Mach-Zehnder modulator (MZM) driven with a sinusoidal at  $f_{RF}/2$  to generate two spectral lines spaced at  $f_{RF}$ . The signal is amplified and an arrayed waveguide grating (AWG) used to separate the two lines while suppressing the central line, allowing one line to be modulated in a second MZM. The latter is driven at data rates of 1 Gbit/s and 2.5 Gbit/s by a  $2^{15} - 1$  bit long pseudo-random bit sequence (PRBS15) non-return-to-zero (NRZ) signal from a pulse pattern generator (PPG). The lines are recombined, amplified and transmitted through 10 km of ITU-T G.652 standard single-mode fiber (SMF) and one of three spool samples of 5 km Sterlite bending insensitive fiber. In order to test the effects of macrobending, the different fibers are wound for 1 to 10 turns around mandrels with radii between 5 mm and 15 mm while monitoring the resulting incident power on the photodiode (PD) with a 1 % tap and recording bit-error rate (BER) values after wireless transmission. It should be noted that the impact of macrobending and the performance analysis of the BIF are independent of the choice of signal generation scheme.

The beating of the two signal lines on the PD generates the radio-frequency (RF) signal at  $f_{RF} = 84$  GHz which is transmitted wirelessly over a distance of 70 m with a pair of parabolic antennas—with a gain of 48 dBi each. A low noise amplifier (LNA) with 40 dB gain restores the signal level before the receiver which consists of a Schottky diode based envelope detector (ED) and digital storage oscilloscope (DSO). With only a single LNA and the use of envelope detection rather than down-conversion with an electrical mixer the need for a local oscillator at the receiver is alleviated and the complexity in the RF domain is kept to a minimum. Finally BER values are determined through offline processing, consisting of simple thresholding and error counting over four recorded sequences with a combined length  $> 10$  Mbit.

Fig. 2 gives an overview of the laboratory setup with optical signal generation, bending test and receive antenna co-located

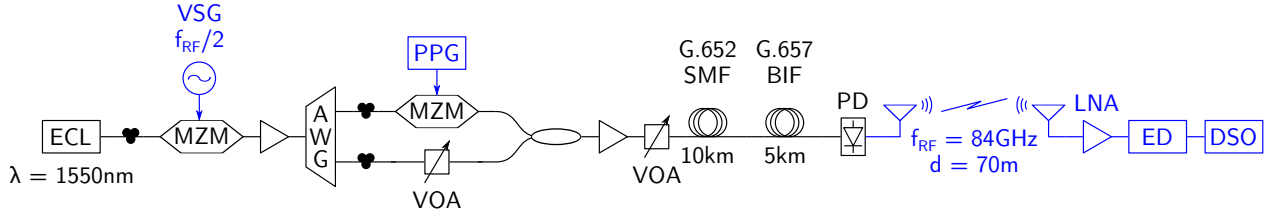


Fig. 1. Experimental setup for radio-over-fibre transmission including bend insensitive fibre. ECL: external cavity laser, VSG: vector signal generator, MZM: Mach-Zehnder modulator, AWG: arrayed waveguide grating, PPG: pulse pattern generator, VOA: variable optical attenuator, PD: photodiode, LNA: low noise amplifier, ED: envelope detector, DSO: digital storage oscilloscope

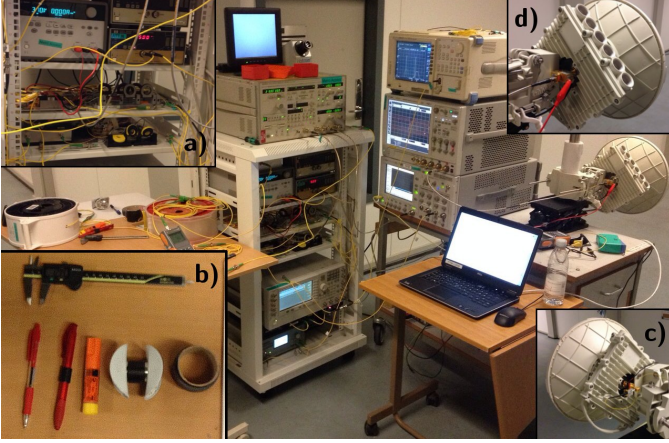


Fig. 2. Portable laboratory setup with photonic upconversion. Insets: a) Rack-mounted optical setup, b) Mandrels of different radii, c) Transmit antenna with PD, d) Receive antenna with LNA and ED

for experiment convenience while the transmit antenna and attached PD are remotely fed through an optical fiber.

### III. EXPERIMENTAL RESULTS

In this work the performance of a hybrid optical-wireless link is analyzed in the presence of fiber bends similar to what would be found in a fiber installation at a radio-access-unit or the antennae of a wireless broadband access link. First the macrobending loss performance of the different fibers under test is compared to the specification for bend insensitive fiber (BIF) of ITU-T G.657, with results shown in Fig. 3. The tested sample A shows macrobending losses significantly—as much as an order of magnitude at radii of 10 mm and 15 mm—below those of SMF and well below those required by ITU-T G.657.A1. Samples B and C show similar performance at a bending radius of 5 mm with sample C showing a five times lower loss at 7.5 mm radius; both show loss figures below the requirements set by G.657.A2/B2 and sample C further meets the loss requirements of G.657.B3.

As the number of bends in an installation may easily add up to the equivalent of five to ten turns, these loss figures indicate that while at a radius of 15 mm the bending loss introduced by SMF may be tolerable, category G.657.A1 fiber will be required at 10 mm and A2/B2 or B3 fiber for even smaller radii in order to remain within typical system power budgets.

Fig. 4 a) and Fig. 5 a) show the dependency of system BER performance on the optical power  $P_{PD}$  incident on the PD at 1 Gbit/s and 2.5 Gbit/s respectively. Setting  $P_{PD} = 6$  dBm

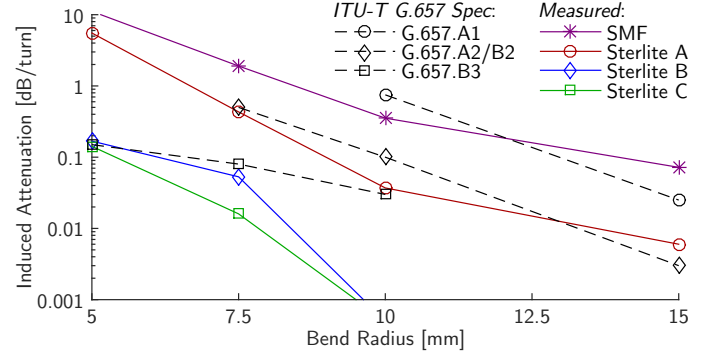


Fig. 3. Comparison of macrobending losses of Sterlite BIF fiber samples at 1550 nm with ITU-T G.657 A1, A/B2 and B3 specifications

as reference power and assuming a required maximum BER of  $10^{-6}$  gives an allowable margin of just below 2 dB for loss induced by fiber bending, with a near negligible penalty for going from 1 Gbit/s to 2.5 Gbit/s.

With the same BER limit and data rates the combinations of fibers, radii and numbers of turns that have been found to be allowable while maintaining system performance are shown in Fig. 4 b) and Fig. 5 b) respectively.<sup>1</sup> The benefit obtained by the use of G.657 fibers is immediately visible at both data rates and it is evident that especially for small radii category A2/B2 and B3 fiber will be a necessity. The observed maximum allowable combinations together with the loss/turn values from Fig. 3 adhere to the allowable loss margin of about 2 dB derived from Fig. 4 a) and Fig. 5 a). While no difference between sample B and C fibers is observed in either Fig. 4 b) or Fig. 5 b), an extrapolation of the number of turns up to the found acceptable loss margin suggests respective allowable numbers of turns of 11 and 14 at 5 mm and 38 and 126 at 7.5 mm, clearly showing the benefit of a fiber with bending loss as low as found for sample C when considering complex installations.

While the margin of 2 dB for allowable bending loss is specific to the assessed system and link, the trade-off it highlights is a general one, requiring assessment of system parameters such as the available power budget, logistical challenges such as the required tolerance to bending and ease of installation as well as economical considerations such as the additional cost of BIF. Due to the drastic differences in loss however these considerations are likely to be between the different types of

<sup>1</sup>Setting a BER limit of  $10^{-3}$  does not significantly alter the picture with only a single data point being changed for each of the data rates as indicated by the  $\nabla$  in Fig. 4 b) and  $\triangle$  in Fig. 5 b).

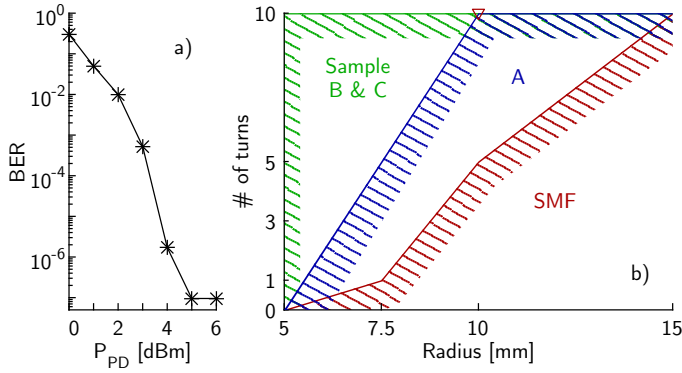


Fig. 4. a) BER vs  $P_{PD}$  at 1 Gbit/s without bending, b) Allowable radii and numbers of turns for a system performance with  $BER < 10^{-6}$  at 2.5 Gbit/s ( $\nabla$ :  $BER = 2.0 \cdot 10^{-4}$  for 10 turns @ 10 mm with SMF fiber)

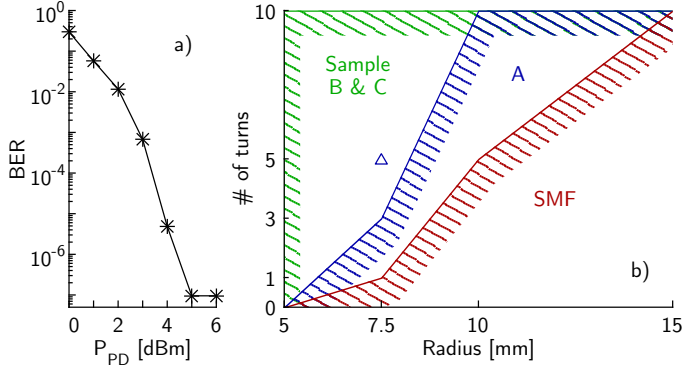


Fig. 5. a) BER vs  $P_{PD}$  at 2.5 Gbit/s without bending, b) Allowable radii and numbers of turns for a system performance with  $BER < 10^{-6}$  at 2.5 Gbit/s ( $\Delta$ :  $BER = 2.5 \cdot 10^{-6}$  for 5 turns @ 7.5 mm with sample A)

BIF rather than whether or not BIF will be included for the last stretch of fiber in the on-site and antenna installation.

#### IV. CONCLUSIONS

We assessed the performance of a W-band hybrid fiber-wireless link with 70 m wireless and 15 km fiber transmission distance under the inclusion of 5 km of bend insensitive fiber (BIF), matching the scenarios for mobile fronthaul or wireless broadband access.

A selection of BIFs were verified to adhere to and actually outperform the requirements set by ITU-T G.657. With these the impact of fiber bending at radii between 5 mm and 15 mm on system performance has been analyzed and the trade-off between available power budget and required tolerance to bending has been discussed both with respect to the presented system as well as in general terms.

The observed loss difference between SMF and BIF suggests the inclusion of BIF as a key enabler for RoF solutions for next generation mobile fronthaul and wireless broadband access where fiber bending is unavoidable due to on-site and antenna installation. The demonstrated benefit of BIF is available to RoF in any frequency band and may be harnessed in combination with wavelength division multiplexing.

#### ACKNOWLEDGMENTS

The authors wish to thank Siklu Communication Ltd. for providing the W-band antennas.

This work was partly funded by the DFF FTP mmW-SPRAWL and EC IPHOAC-NG projects. L. Cavalcante thanks the Brazilian government for supporting his research through the Science without Borders program.

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